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# First measurements of the absolute neutron spectrum using the Magnetic Recoil Spectrometer (MRS) at OMEGA

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A new type of neutron spectrometer, called a Magnetic Recoil Spectrometer (MRS), has been built and implemented at the OMEGA laser facility [T. R. Boehly, D. L. Brown, R. S. Craxton *et al.*, *Opt. Commun.* **133**, 495 (1997)] for absolute measurements of the neutron spectrum in the range 6 to 30 MeV, from which fuel areal density ( $\rho R$ ), ion temperature ( $T_i$ ) and yield ( $Y_n$ ) can be determined. The results from the first MRS measurements of the absolute neutron spectrum are presented. In addition, measuring  $\rho R$  at the National Ignition Facility (NIF) [G.H. Miller, E.I. Moses and C.R. Wuest, *Nucl. Fusion* **44**, S228 (2004)] will be essential for assessing implosion performance during all stages of development from surrogate implosions to cryogenic fizzles and ignited implosions. To accomplish this, we are also developing an MRS for the NIF. As much of the R&D and instrument optimization of the MRS at OMEGA is directly applicable to the MRS at the NIF, a description of the MRS design on the NIF is discussed as well.

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## I. Introduction

Proper assembly of capsule mass, as manifested through evolution of fuel areal density ( $\rho R$ ),<sup>1-3</sup> is fundamentally important for achieving hot-spot ignition planned at the National Ignition Facility (NIF).<sup>4</sup> Experimental information about  $\rho R$  and  $\rho R$  asymmetries, as well as  $T_i$  and yield is therefore absolutely essential for understanding how assembly occurs and critically evaluating numerical simulations during all stages of development from surrogate implosions to cryogenic fizzles to ignited implosions. To accomplish this, we are currently developing a new type of neutron spectrometer, a Magnetic-Recoil Spectrometer (MRS), whose objective is to measure the absolute spectrum in the range 6 to 30 MeV, from which  $\rho R$ ,  $T_i$  and yield can be directly inferred. Important to the design is that the MRS covers all essential details of the neutron spectrum. A fuel  $\rho R$  can be inferred from the measured spectrum of the down-scattered neutrons in the range 6-10 MeV. Measurements of the tertiary spectrum ( $>20$  MeV) allow a second determination of the  $\rho R$  for high-yield implosions, which can be compared directly to the down-scattered neutron inferred  $\rho R$ . Having such self-consistency check could prove immensely important for NIF fizzles that are on the threshold to ignite. In addition,

absolute yield and a highly resolved 14 MeV primary neutron spectrum can be measured. This allows for measurements of  $T_i$  and, possibly more interestingly, non-thermal features, deviations from a single temperature and the effect of alpha-particle heating that might give an insight into the nature of a failed ignition-capsule implosions that have, for example, a substantial cold high-density plasma that surrounds a hot low-density plasma.

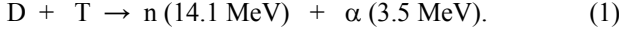
A prototype MRS has been built on OMEGA<sup>5</sup> to comprehensively test the technique, and, from the experience gained at OMEGA, insightfully design an optimal MRS for the NIF. There are other important reasons for taking this approach. First,  $\rho R$  of both surrogate and cryogenic DT implosions can be inferred from both the MRS and charged-particle spectrometry [with knock-on deuterons (KO-D)] for moderate  $\rho R$  implosions ( $\rho R < 200$  mg/cm<sup>2</sup>);<sup>6-8</sup> this allows for a definitive check of the MRS. Second, as there are no other ways to determine cryogenic  $\rho R > 200$  mg/cm<sup>2</sup> at OMEGA, the MRS brings the required diagnostic to the OMEGA cryogenic program.

This paper is structured as follows: Section II describes the Inertial Confinement Fusion (ICF) neutron spectrum and how it can be used to determine  $\rho R$ ,  $T_i$ , multi- $T_i$ , non-thermal features, the effect of  $\alpha$ -particle heating and neutron yield ( $Y_n$ ). Section III and IV discusses the design

and characterization, respectively, of the MRS at OMEGA and the NIF. Section V presents the results from the first measurements of the neutron spectrum using the MRS at OMEGA, while Section VI presents MRS measurements of KO-D spectrum, from which  $\rho R$  can be directly inferred. Section VII summarizes the paper.

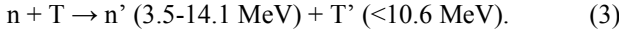
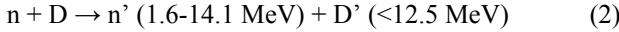
## II. The ICF neutron spectrum

In an ICF implosion, primary neutrons are produced primarily via the reaction



The primary DT neutrons carry a wealth of information about the ICF implosion, such as information about  $T_i$ , multi- $T_i$ , possible non-thermal features and  $Y_n$ .<sup>9</sup> For a single-temperature plasma,  $T_i$  can be determined from the Doppler width ( $\Delta E_D$ ) of the primary neutron spectrum [to the first order  $T_i \approx (\Delta E_D/177)^2 \text{ keV}$ ],<sup>9</sup> which is represented accurately by a single-Gaussian distribution. The effect of multi- $T_i$  (caused by for instance temperature profiles) and non-thermal features would simply show up as deviations from the single-Gaussian distribution. The non-thermal feature could, for instance, be generated by a strong, localized electrical field, which originates from the pressure gradient inside the implosion<sup>10</sup> causing strong bulk flows at high velocities on the order of the sound speed.

In a secondary process, a small fraction of the primary neutrons elastically scatter off the fuel ions [primarily deuterons (D) and tritons (T)] as described by

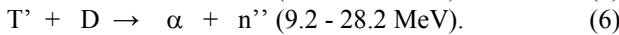
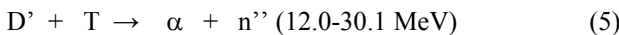


By using a relatively simple model of an implosion, the  $\rho R$  can be related to the down-scattered neutron yield ( $Y_n$ ) by

$$\rho R \approx \frac{(2\gamma + 3)m_p}{(\gamma\sigma_d + \sigma_t)} \frac{Y_{n'}}{Y_n} \quad (4)$$

where  $\gamma = n_d/n_i$ ,  $\sigma_d$ , and  $\sigma_t$  are the effective elastic scattering cross sections for deuterons and tritons, respectively;  $m_p$  is the proton mass;  $Y_{n'}$  is the measured down-scattered neutron yield in a certain defined energy range; and  $Y_n$  is the measured primary neutron yield. As shown by Eq. (4), the fuel  $\rho R$  is linearly proportional to yield ratio of down-scattered neutrons ( $n'$ ) and primary neutrons ( $n$ ).<sup>8</sup>

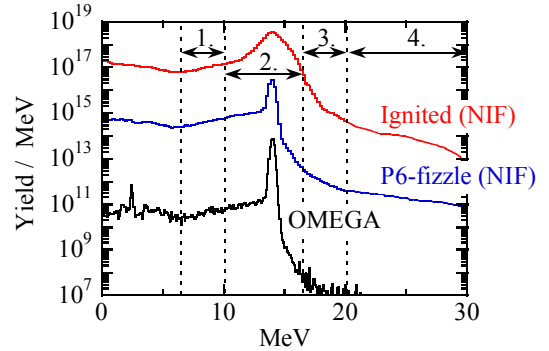
As scattered high-energy deuterons ( $D'$ ) or tritons ( $T'$ ), produced in process (2) and (3), pass through the fuel, some undergo tertiary reactions and produce tertiary neutrons ( $n''$ )



According to LASNEX simulations,<sup>11</sup> the yield of the tertiary neutrons ( $> 20 \text{ MeV}$ ) is of the order  $10^{-6}$  relative to the primary neutron yield, and proportional to  $\rho R$  and  $\rho R^2$  for high- $\rho R$  and low- $\rho R$  implosions, respectively.

When the alpha particles, produced in reaction (1), interact with the plasma they lose energy mainly through small angle scattering with electrons. However, there is a finite probability that the alpha particles transfer energy to the D's or T's of several MeV by large angle Coulomb or nuclear-elastic scattering. These collisions give rise to non-thermal distributions of fuel ions, which can in turn react with the thermal ions generating a secondary component in the neutron spectrum. Although with much lower intensity than the primary component ( $\sim 10^{-5}$  to  $\sim 10^{-2}$  depending on the implosion), the secondary-neutron component dominates at energies in the range 16-20 MeV. As the intensity of the secondary-neutron component is strongly sensitive to electron temperature ( $T_e$ ), measurement of this component could, in principle, address  $T_e$  in the high-density region, the effect of alpha-particle heating and fuel-ablator mix.

A few typical neutron spectra simulated by LASNEX for OMEGA and the NIF are shown in Fig. 1. These spectra are based on all possible reaction processes starting with the DT and DD reaction. A fuel  $\rho R$  can be inferred from the down-scattered neutrons in region 1.  $T_i$ , multi- $T_i$ ,  $Y_n$ , possible non-thermal features can be determined from the primary peak in region 2. The effect of alpha-particle interaction with thermal fuel ions can be determined from the secondary neutrons in region 3, and a second  $\rho R$  for high-yield implosions can be derived from the tertiary neutron spectrum in region 4.

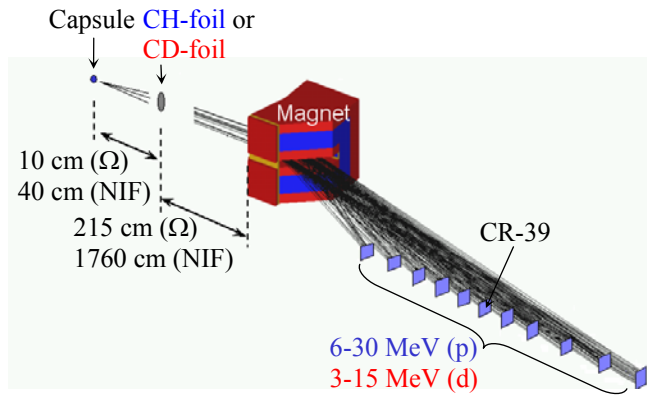


**Figure 1:** Typical neutron spectra simulated by LASNEX for an OMEGA (black line) and two NIF (blue and red lines) cryogenic DT implosions. For OMEGA, a primary neutron yield of  $2.4 \times 10^{13}$  and down-scattered neutron yield of  $1.5 \times 10^{11}$  (region 1) corresponding to a fuel  $\rho R$  of  $128 \text{ mg/cm}^2$  were simulated. For NIF, a neutron spectrum was simulated for an ignited (red line) and a P<sub>6</sub>-fizzle (blue line) implosion. For the ignition case, a primary yield of  $7.4 \times 10^{18}$  and down-scattered yield of  $3.6 \times 10^{17}$  were simulated. A significant tertiary component (region 3) of  $1.5 \times 10^{15}$  was simulated as well. For the “P<sub>6</sub> fizzle”, a primary yield of  $2.1 \times 10^{16}$ , down-scattered yield of  $1.5 \times 10^{15}$  and tertiary yield of  $2.0 \times 10^{12}$  were simulated. A  $\rho R$  of  $\sim 2 \text{ g/cm}^2$  was simulated in both cases. The non-thermal, secondary-neutron component, originating from the alpha-particle interaction with the fuel ions, dominates at energies in the range 16 - 20 MeV (region 2). A secondary-neutron yield of  $1.5 \times 10^8$ ,  $6.8 \times 10^{12}$  and  $9.0 \times 10^{16}$  was simulated for the OMEGA, NIF-P<sub>6</sub>-fizzle and the NIF-ignition implosion, respectively.

## III. Design of the MRS at OMEGA and the NIF

The MRS has three main components (see Fig. 2). The first component is a CH (or CD) foil positioned as close

as possible to the implosion,<sup>12</sup> to produce recoil protons (or deuterons) from incident neutrons. The second component is a focusing magnet, located outside the target chamber in the case of OMEGA, and located outside the target-bay area in the case of the NIF,<sup>13</sup> for energy dispersion and focusing of forward-scattered recoil particles onto the focal plane of the spectrometer. The focusing provides a clear mapping between position at the focal plane and energy of the proton (or deuteron), and thus the energy of the neutron that scattered it. The third component is an array of CR-39 detectors, positioned at the focal plane of the spectrometer, which record the position of each recoil particle with a detection efficiency of 100%.<sup>14</sup> By measuring the recoil-particle spectrum, the neutron spectrum is indirectly measured as the MRS response function is well known.



**Figure 2:** A schematic drawing of the MRS, including the foil, magnet, and CR-39 detectors. The foil is positioned as close as possible to the implosion (10 cm in the case of OMEGA and 40 cm in the case of the NIF); the magnet is positioned outside the target chamber in the case of OMEGA (215 cm to the foil), and outside the target-bay wall in the case of the NIF (1760 cm to the foil). Important to the MRS design is that the same magnet design can be used on OMEGA and the NIF. In the case OMEGA, eleven  $6 \times 5$  cm<sup>2</sup> CR-39 detectors are positioned at the focal plane of the spectrometer for detection of the forward scattered recoil protons (or deuterons) when using a CH foil (or CD foil). The trajectories shown are for proton energies from 6 to 30 MeV, corresponding to deuteron energies from 3 to 15 MeV. For protons, the dispersion is  $\sim 30$  keV/mm at 6 MeV and  $\sim 70$  keV/mm at 25 MeV. These numbers are reduced with a factor of two for the deuterons.

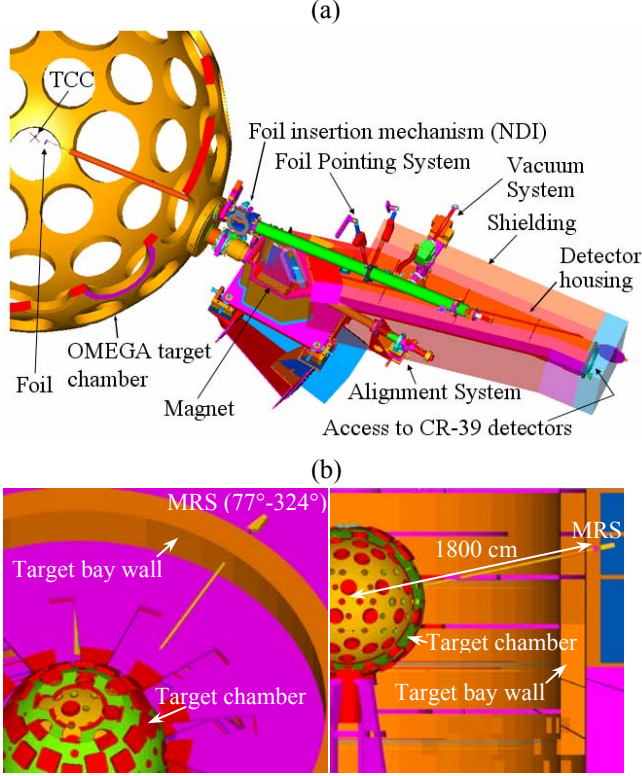
An important characteristic to the MRS design is that the detection efficiency ( $\epsilon_{MRS}$ ) for a given response function [energy resolution ( $\Delta E_{MRS}$ )] is maximized. This is achieved by using an aperture in front of the magnet that selects recoil particles scattered in the forward direction at which the nd- and np-differential elastic scattering cross sections have their maximums in the laboratory system and  $\Delta E_{MRS}$  has its minimum due to shortest average path length of the recoil particles in the foil.<sup>15</sup> In this context, it is also important to note that the magnet, which is made of Neodymium-Iron-Boron (NdFeB), is a focusing device with a pole gap of 3 cm producing a magnetic field up to  $\sim 0.9$  Tesla and a field gradient of  $\sim 60$  Gauss/cm. The entrance and exit pole boundaries are also angled relative to the incoming and outgoing particles, as discussed in principle in ref. <sup>15</sup>, for increased focusing properties in both the transverse and

dispersive planes, where the former prohibits the recoil particles from hitting the pole boundaries, and latter provides for increased resolving power. These features are critical to the MRS design as they allow for the largest possible solid angle to be used, which maximizes  $\epsilon_{MRS}$  for a defined  $\Delta E_{MRS}$ .

For the MRS to be both practical and useful at OMEGA and the NIF, it has been designed with the highest possible  $\epsilon_{MRS}$  for a given  $\Delta E_{MRS}$ , the largest possible dynamic range, and insensitivity to different types of background. Built-in flexibility has also been included in the design to effectively use the MRS for different applications. This is important, as a tradeoff between  $\epsilon_{MRS}$  and  $\Delta E_{MRS}$  must be applied depending on the application. For instance, for a practical implementation of low-yield applications, such as measurements of down-scattered and secondary neutrons at OMEGA for which yields are orders of magnitude smaller than the primary yield (see Fig. 1), it is necessary to degrade  $\Delta E_{MRS}$  to substantially increase  $\epsilon_{MRS}$ . For high-yield applications, on the other hand, such as measurements of primary neutron spectrum at OMEGA and the NIF, the MRS can be configured to operate in a high-resolution-low- $\epsilon_{MRS}$  mode. Several options are available for configuring the MRS. Either a CH or CD can be selected to produce recoil protons or deuterons (and thus whether the energy range covered for neutrons is 6 – 30 MeV or 3.4 – 16.9 MeV). The foil area and thickness can be adjusted to change the  $\epsilon_{MRS}$  and  $\Delta E_{MRS}$ . The area of the aperture in front of the magnet can be adjusted as well.

As CR-39 detectors are used in the MRS, the principal sources of background are primary neutrons and neutrons scattered by the chamber wall, diagnostics, and other structures surrounding the MRS. Soft and hard x rays are not an issue, since CR-39 is immune to these types of radiation. Although the CR-39 efficiency for detecting primary neutrons is small<sup>16</sup> ( $\epsilon_{CR-39} \approx 6 \times 10^{-5}$ ), reduction of the neutron background is required for successful implementation of the MRS down-scattered neutron measurements. To reduce the neutron background to the required level for down scattered neutron measurements at OMEGA,<sup>17</sup> polyethylene shielding was applied to the MRS as a first step. As the CR-39 detector array is positioned on an off-axis detection plane that is well outside the target chamber, enough space exists to position  $\sim 2200$  lbs of polyethylene shielding in front and around the MRS. A 60 lb stainless steel plug was also placed in between the implosion and the MRS detector array to allow additional attenuation of direct, primary neutrons because of the relatively high inelastic scattering cross-sections in Iron, Chromium and Nickel. Through measurements and neutron-transport simulations using the Monte-Carlo code TART,<sup>18</sup> we have established that the shielding reduces the neutron fluence  $\sim 40$  times to a fluence of  $\sim 2 \times 10^{-8}$  cm<sup>-2</sup> per produced neutron at the MRS detector array.<sup>19</sup> Fig. 3a shows the final engineering design of the MRS on OMEGA. In contrast, shielding around the MRS is not required at the NIF as the system is protected by 1.8 m of concrete (see Fig. 3b).<sup>17</sup>





**Figure 3:** (a) Engineering design of the MRS on OMEGA. The foil is inserted by the Nuclear Diagnostics Inserter (NDI) to 10 cm from target-chamber center (TCC). The MRS magnet, magnet housing, detector housing and shielding are shown in the figure. The total weight of the MRS is ~4100 lbs including the ~2200 lbs of polyethylene shielding. (b) Conceptual design of the MRS on the NIF. The current plan is to position the MRS outside the target-bay wall (1.8 m of concrete) on the line-of-sight 77°- 324°.

For successful implementation of the down-scattered neutron measurements at OMEGA, additional reduction of the neutron background is required. This is accomplished through the use of the Coincidence Counting Technique (CCT), which utilizes the fact that incident signal particles pass straight through the CR-39, if it is thin enough, resulting in coincident front-side and back-side tracks. Real signal tracks can therefore be distinguished easily from neutron-induced events, as the latter events produce only a track on either the front or back side of the CR-39. When applying the CCT to the MRS data, the  $S/B$  ratio can be expressed as<sup>17</sup>

$$\left(\frac{S}{B}\right)_{CCT} \approx \frac{A}{\pi r_c^2} \frac{S}{(S+B)^2}, \quad (7)$$

where  $A$  is the signal-detection area,  $r_c$  is the correlation radius used when searching for coincident front-side and back-side tracks,  $S$  is number of signal events produced by down-scattered neutrons in the energy range 6-10 MeV, and  $B$  is the number of background events observed in the detection area. For low signal and background track densities, the  $(S/B)_{CCT}$  ratio is typically of the order  $10^2$ - $10^3$ ; a result of the fact that  $A/\pi r_c^2$  is a large number. As the signal and background track densities increase, the  $(S/B)_{CCT}$

ratio decreases due to an increasing number of random coincidences. In addition, it should be noted that the CCT does not have to be applied to the down-scattered neutron data obtained at the NIF, as the MRS is behind 1.8 m of concrete (see Fig. 3b), which is thick enough to reduce the neutron background to an acceptable level of  $\sim 5 \times 10^{-12} \text{ cm}^{-2}$  per produced neutron.  $S$  and  $B$  in Eq. (7) can be expressed as<sup>17</sup>

$$S \approx 0.03 \cdot \rho R [\text{g/cm}^2] \cdot Y_n \cdot \epsilon_{MRS}, \quad (8)$$

$$B \approx 2 \times 10^{-8} \cdot A \cdot Y_n \cdot \epsilon_{CR-39}, \quad (\text{OMEGA}) \quad (9)$$

$$B \approx 5 \times 10^{-12} \cdot A \cdot Y_n \cdot \epsilon_{CR-39}. \quad (\text{NIF}) \quad (10)$$

Here,  $\epsilon_{MRS}$  is discussed in section IV, and  $A$  is  $\sim 75$  and  $\sim 25 \text{ cm}^2$  for the down-scattered neutron measurements at OMEGA and the NIF, respectively. For primary neutron measurements, Eq. (8) should be modified to  $S \approx Y_n \cdot \epsilon_{MRS}$ .

#### IV. Characterization of the MRS at OMEGA and the NIF

GEANT4<sup>20</sup> and a developed Monte-Carlo code were used to characterize the performance of the MRS when operating in different configurations at OMEGA and the NIF. The results from that modeling are shown in Table 1 for the down-scattered neutron measurements in the energy range 6-10 MeV. The first and second column is for the MRS operating in a high- $\epsilon_{MRS}$  and low- $\epsilon_{MRS}$  mode at OMEGA, respectively. The third and fourth column is for the MRS operating in a low- $\epsilon_{MRS}$  and high- $\epsilon_{MRS}$  mode at the NIF, respectively. The difference between the two configurations at OMEGA or the NIF is due to the different characteristics of the foil. For primary neutron measurements,  $\epsilon_{MRS}$  and  $\Delta E_{MRS}$  numbers, shown in Table 1, should be reduced by  $\sim 40\%$ . In addition, the high- $\epsilon_{MRS}$  mode is applied mainly to down-scattered neutron measurements at OMEGA, while low- $\epsilon_{MRS}$  mode is applied normally to high-resolution studies of primary neutron spectrum. High-resolution studies can also be applied to down-scattered neutron measurements when  $Y_n$  is high enough.

**Table 1:** Detection efficiency ( $\epsilon_{MRS}$ ) and energy resolution ( $\Delta E_{MRS}$ ) for two different MRS configurations at OMEGA and the NIF. The first and second column is for the MRS operating in a high- $\epsilon_{MRS}$  and low- $\epsilon_{MRS}$  mode at OMEGA, respectively. The third and fourth column is for the MRS operating in a low- $\epsilon_{MRS}$  and high- $\epsilon_{MRS}$  mode at the NIF, respectively. These numbers are for measurements of down-scattered neutrons when using a CD foil. A factor of two thicker CH foil provides the same  $\epsilon_{MRS}$  and  $\Delta E_{MRS}$ . In addition, the  $\epsilon_{MRS}$  and  $\Delta E_{MRS}$  numbers should be reduced by  $\sim 40\%$  for primary neutron measurements.

Configuration	OMEGA		NIF	
	#1	#2	#1	#2
CD-foil distance [cm]	10	10	40	40
CD-foil thickness [ $\mu\text{m}$ ]	40	290	40	290
CD-foil area [ $\text{cm}^2$ ]	4.0	13	20	20
Magnet aperture [cm]	22	22	20	20
Magnet aperture dist. [cm]	215	215	1760	1760
$\Delta E_{MRS}$ (FWHM) [MeV]	0.5	2.0	0.4	1.8
$\epsilon_{MRS} [\times 10^{-11}]$	35	820	0.15	1.1

The signal-to-noise ( $S/N$ ) and signal-to-background ( $S/B$ ) ratios for the down-scattered neutron measurements at OMEGA and the NIF can now be determined from Eqs. (7) - (10) and Table 1. The results are summarized in Table 2 for a warm DT-filled CH implosion at OMEGA and the cryogenic DT implosions discussed in Section II. It can be seen in Table 2 that the MRS will accurately diagnose the  $\rho R$  for these implosions.

**Table 2:** Signal-to-noise ( $S/N$ ) and signal-to-background ( $S/B$ ) ratios for the different MRS configurations, shown in Table 1, planned to be used for the down-scattered neutron measurements (6-10 MeV) at OMEGA and the NIF. The CCT [Eq. (7)] has only been applied to the OMEGA data when using a correlation radius of 50  $\mu\text{m}$ . As  $Y_n$  is at least two orders of magnitude higher than  $Y_n$ , the  $S/B$  and  $S/N$  ratios for the primary neutron measurements is at least a factor of 100 and 10 higher, respectively.

Facility	Implosion	$\rho R$ [g/cm <sup>2</sup> ]	$Y_n$	$S/N$		$S/B$	
				#1	#2	#1	#2
OMEGA	Warm <sup>8</sup>	0.07	$10^{13}$	3	13	15	230
	Cryo	0.13	$2 \times 10^{13}$	5	25	14	154
NIF	P <sub>6</sub> fizzle	2.0	$2 \times 10^{16}$	42	115	12	88
	Ignited	1.9	$7 \times 10^{18}$	245	2095	11	84

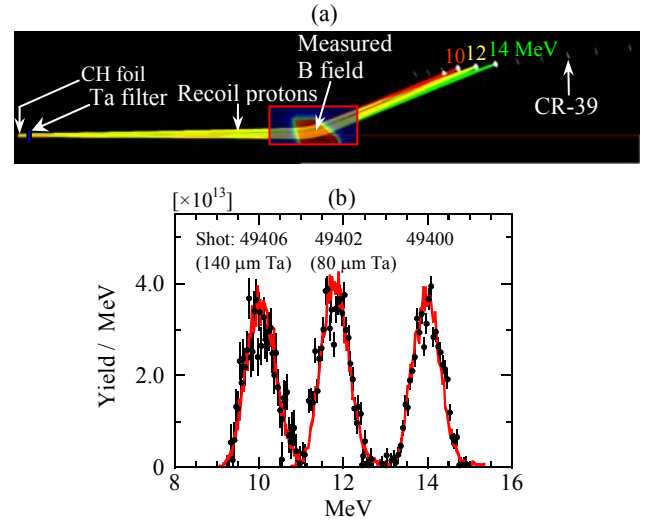
As the CR-39 detects the recoil particles with 100% efficiency and  $B$  is small in comparison, the MRS dynamic range is determined mainly by signal statistics and signal saturation. About  $\sim 10^2$  signal counts are required to infer a fuel  $\rho R$  from the down-scattered neutron spectrum, and  $\sim 10^7$  signal counts over the signal detection area are required for the CR-39 to saturate.<sup>14</sup> This results in a single shot dynamic range of  $\sim 10^5$ . An additional factor of ten is achieved due to the large flexibility built into the design.

## V. MRS activation and calibration experiments

For the MRS activation and calibration experiments, a series of DT filled CH capsules with a nominal diameter of 850  $\mu\text{m}$ , a fill pressure of 15 atm, and shell thickness of 15  $\mu\text{m}$  were imploded with a 1-ns square laser pulse shape delivering  $\sim 23$  kJ of UV-energy on capsule. All laser beams on OMEGA were smoothed with SG3 distributed phase plates,<sup>21</sup> 1-THz, two-dimensional smoothing by spectral dispersion,<sup>22</sup> and polarization smoothing using birefringence wedges.<sup>23</sup> The beam-to-beam energy imbalance was typically 3% rms for these implosions.

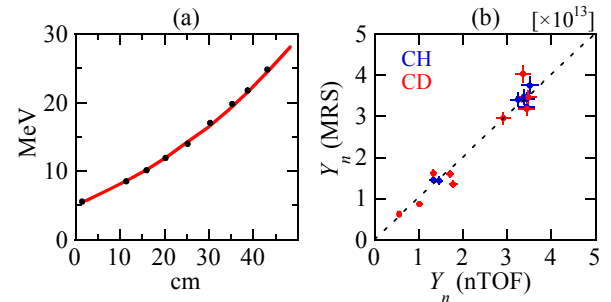
A primary neutron yield from  $\sim 10^{13}$  to  $\sim 3 \times 10^{13}$  and a  $T_i$  in the range 5-6 keV were produced in these implosions. An accurate yield and energy calibration of the MRS could therefore be obtained as these yields were high enough to allow the MRS to operate in a high-resolution mode (configuration #1 shown in Table 1). Twelve implosions were used for these experiments. For each shot, a Tantalum (Ta) filter, with a certain thickness, was positioned just behind the CH (or CD) foil to range down the energy of the recoil protons (or deuterons) (see Fig. 4a). This allowed for an accurate energy calibration of the MRS in the range 6 to 25 MeV (proton equivalent energy). The energies above 14 MeV are accessible using recoil deuterons from a CD-foil. Fig. 4b shows a subset of three measured spectra that are compared to GEANT4 modeling of the MRS. A Ta filter

with thickness 80 and 140  $\mu\text{m}$  was positioned just behind the CH foil to range down the spectrum to 12 MeV and 10 MeV, respectively. As is illustrated in Fig. 4b, excellent agreement exists between measured and simulated yield, average energy and spectral shape, indicating that the GEANT4 modeling of the MRS is accurate.



**Figure 4:** (a) GEANT4 modeling of the MRS activation and calibration experiments using primary neutrons from a DT filled CH-capsule implosion. A Ta filter with thickness 80 and 140  $\mu\text{m}$  was positioned just behind the CH foil to range down the spectrum to 12 MeV and 10 MeV, respectively. (b) Measured and simulated recoil proton spectra. The measured spectra agree with the GEANT4 modeling in terms of yield, average energy and spectral shape, which indicates that the predicted performance of the MRS is accurate. A total primary neutron yield of  $(3.0 \pm 0.3) \times 10^{13}$ ,  $(3.3 \pm 0.2) \times 10^{13}$  and  $(3.0 \pm 0.2) \times 10^{13}$  was determined for the shot 49406, 49402 and 49400, respectively. It is important to note that these calibration measurements were performed without the shielding installed.

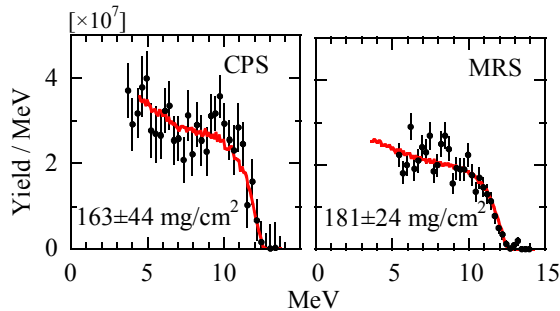
The whole set of MRS data obtained during these experiments is illustrated in Fig. 5. The measured and simulated average energy as a function of position along the focal plane are shown in Fig. 5a, and the MRS determined yields contrasted to the nTOF yields are shown in Fig. 5b. Both sets of data indicate clearly that the MRS performance is well understood, both in terms energy and  $\epsilon_{MRS}$  for practically the whole energy band width of the MRS.



**Figure 5:** (a) Measured and simulated average energy versus position along the focal plane. (b) Yields measured by MRS and nTOF. Both sets of data indicate clearly that the MRS performance is well understood for practically the whole energy band width.

## VI. $\rho R$ measurements using the MRS

MRS measurements of particles produced in secondary processes [Eq. (2) and (3)] have just begun. In particular, spectra of KO-D for cryogenic DT implosions have been obtained by the MRS when it is operating in a charged-particle mode (no foil close to the implosion). An example of the resulting data from those measurements is shown in Fig. 6, and compared to data taken by a standard charged-particle spectrometer (CPS).<sup>14</sup> From the shape of the KO-D spectrum, it has been established through Monte-Carlo modeling of a cryogenic DT implosion that the fuel  $\rho R$  can be determined accurately from the shape of the knock-on deuteron (KO-D) spectrum.<sup>24</sup>



**Figure 6:** CPS and MRS measured KO-D spectra for the low-yield, low-adiabat cryogenic DT implosion 50515. Also shown are simulated fits (red lines) to the measured spectra. From the fits,  $\rho R$ 's of  $163 \pm 44$ , and  $181 \pm 24$  were determined from the CPS and MRS data, respectively.

## VII. Summary

A new type of neutron spectrometer, called a Magnetic Recoil Spectrometer (MRS), has been built and implemented at the OMEGA laser facility for absolute measurements of the neutron spectrum in the range 6 to 30 MeV, from which fuel areal density ( $\rho R$ ), ion temperature ( $T_i$ ) and yield ( $Y_n$ ) can be determined. The results from the MRS activation and calibration experiments, using primary neutrons, indicate that the MRS performs as predicted. With the MRS shielding installed, particles from secondary reactions have now been measured as well. From spectral measurements of KO-D's, fuel  $\rho R$  of a cryogenic DT implosion has been inferred. These types of measurements indicate that the MRS concept will work for the down-scattered neutron measurements at OMEGA and, in particular, at NIF as yields and  $\rho R$ s will be significantly higher. At the NIF, non-thermal features may be explored further to higher levels of accuracy that might give a better insight into the nature of failed ignition-capsule implosions.

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12. The foil needs to be positioned as close as possible to the implosion for a couple of reasons as discussed in ref. 15. First, the detection efficiency for a defined energy resolution is maximized. Secondly, the number of incoming neutrons, at the foil, that have scattered off the target chamber and internal structures is negligible in comparison to the number of down-scattered neutrons coming from the implosion.
13. The magnet is positioned well outside the target chamber in the case of OMEGA and outside the target-bay wall in the case of the NIF to allow for significant amount of shielding to be placed in front and around the MRS.
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